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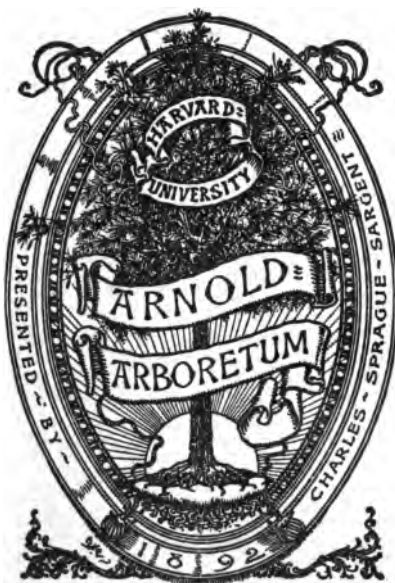
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HENRY S. GRAVES, Forester

FOREST PRODUCTS LABORATORY, Madison, Wisconsin
In Cooperation with the University of Wisconsin

Washington, D. C.

PROFESSIONAL PAPER

July 16, 1919

**THE RELATION OF THE SHRINKAGE
AND STRENGTH PROPERTIES OF
WOOD TO ITS SPECIFIC GRAVITY**

By

J. A. NEWLIN, in Charge, Section of Timber
Mechanics, and T. R. C. WILSON, Engineer in
Forest Products

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PURPOSE.

It has long been recognized that there are direct relations between the specific gravity, or density, of a wood and its strength properties.¹ By the analysis of over 200,000 tests, the Forest Products Laboratory, conducted in cooperation with the University of Wisconsin, Madison, Wis., has now definitely established these relations. It is the purpose of this bulletin to state these relations and to put the expression of them in such form as to render them easily useful (1) for estimating the properties of any particular timber; (2) for selecting timber for any given purpose; (3) for comparing the various species; and (4) for determining in what way the species are exceptional and to what uses they are best adapted.

It has usually been assumed that the strength of wood varies directly with the first power of its density; i.e., that the respective strengths of two sticks would differ in the same proportion as the densities. It was recognized that fiber stress at elastic limit in compression perpendicular to the grain, or bearing strength on side

¹ Accurate determinations made at the Forest Products Laboratory on seven species of wood, including both hardwood and coniferous species, showed a range of only about 4½ per cent in the density of the wood substance, or material of which the cell walls are composed. Since the density of wood substance is so nearly constant, it may be said that the density or specific gravity of a given piece of wood is a measure of the amount of wood substance contained in it.

surface, and work values in static bending or toughness, deviate very erratically from this relation; but the relation was supposed to hold especially true in the case of such properties as modulus of rupture, or maximum bending strength, and strength in compression parallel

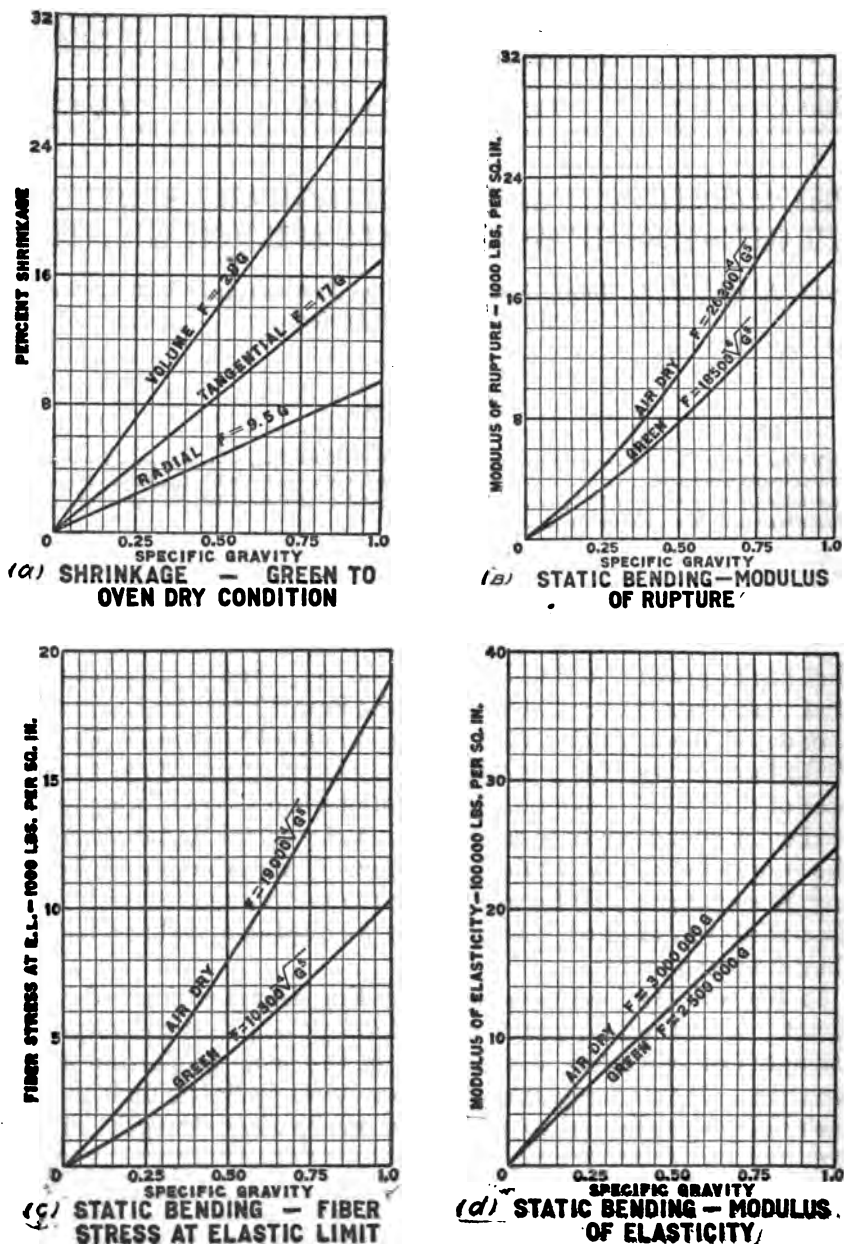


FIG. 1.

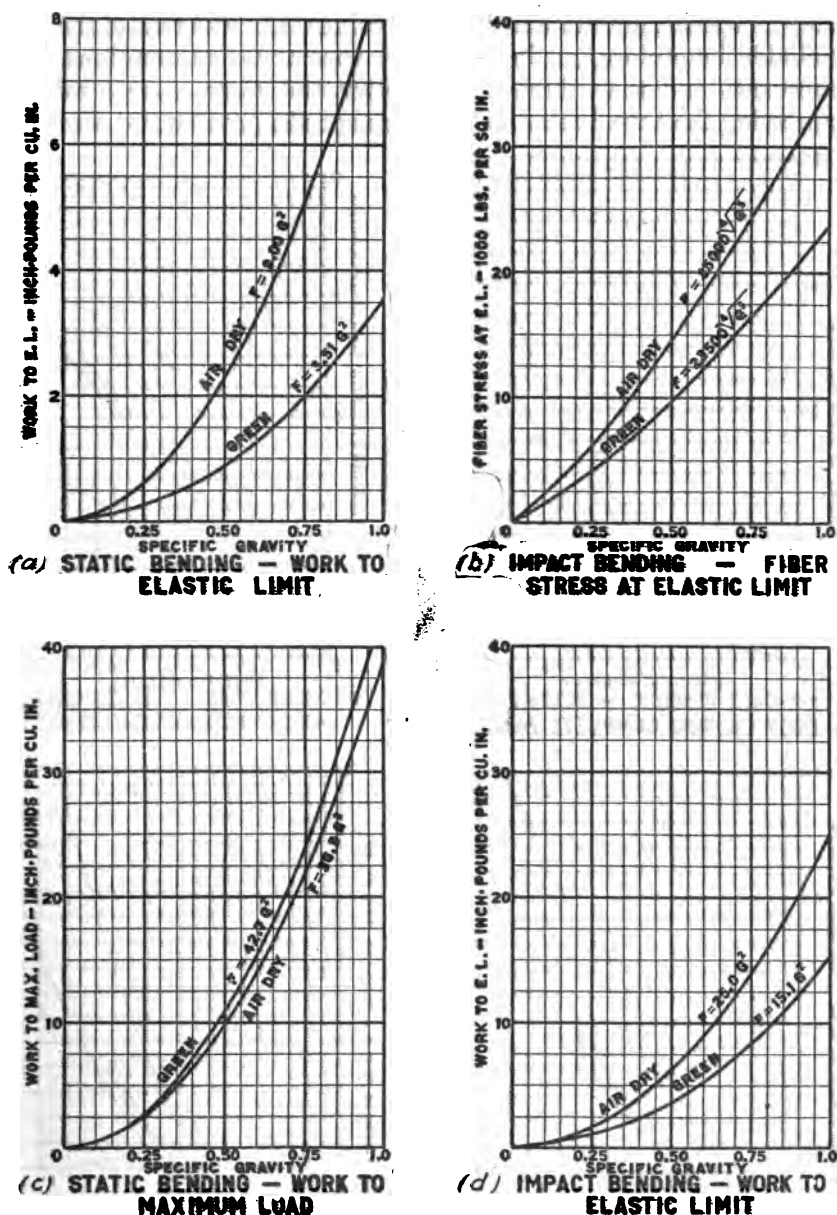
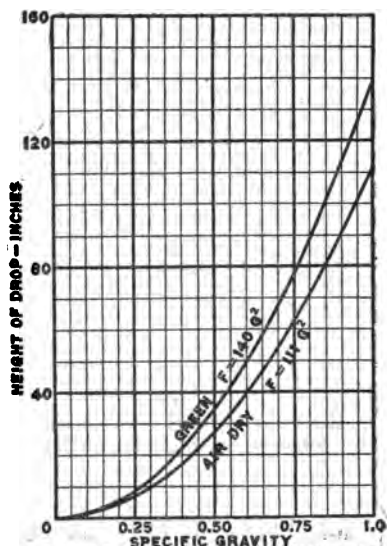


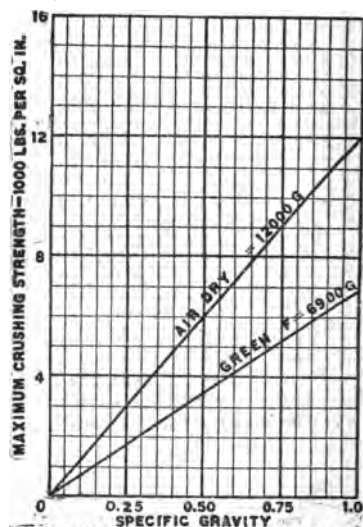
FIG. 2.

to the grain, or strength as a column. It has also been supposed that the relation applied between pieces of the same species, between pieces of different species, and between average results of strength tests on different species. A study of the data at present available, which are derived from a much larger number of tests and which cover a greater

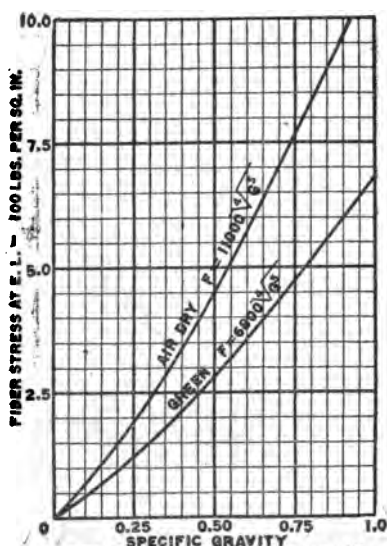
range in specific gravity and strength values than was true of the data available heretofore, made it evident that these assumptions were inaccurate and that there was a better and more correct method expressing the actual relations between specific gravity and strength.



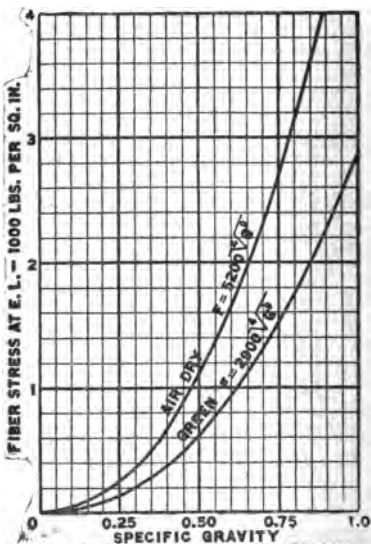
(a) IMPACT BENDING — HEIGHT OF DROP CAUSING COMPLETE FAILURE



(b) COMPRESSION II TO GRAIN
MAXIMUM CRUSHING STRENGTH



(c) COMPRESSION II TO GRAIN
FIBER STRESS AT ELASTIC LIMIT



(d) COMPRESSION I TO GRAIN
FIBER STRESS AT ELASTIC LIMIT

FIG. 3.

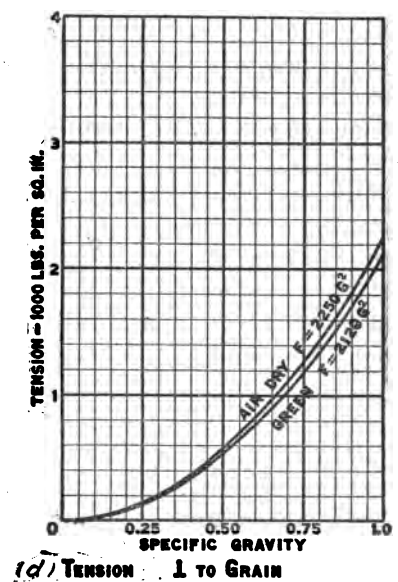
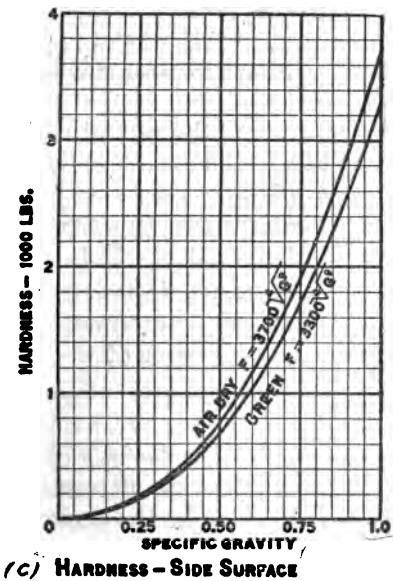
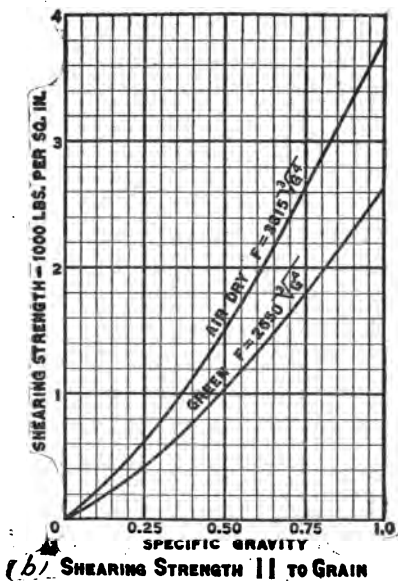
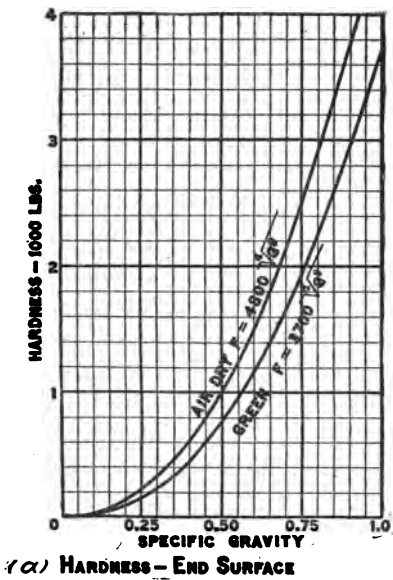


FIG. 4.

In order that the relation between specific gravity and each of the various mechanical properties of wood may be easily put to practical use, the relation, both for green and for air-dry material, is given in the form of an equation (Table 1) and, in addition, in the form of a curve (figs. 1 to 4).

SPECIES-LOCALITY AVERAGES.

The specific-gravity relations given in this bulletin are derived from a study of what may be called "species-locality" averages; that is, each average represents tests of material of one species from one locality.

There are two principal reasons for using "species-locality" averages in preference to the results of individual tests. First, the number of individual tests is quite large, amounting in some instances to as many as 900 from a single "species-locality", so that an immense amount of work is saved by the use of the "species-locality" averages; second, if individual tests were used, the "species-localities" having larger trees or a larger number of trees would include a larger number of tests and would have undue weight in determining the relations.

The method of analysis used is applicable also to individual tests from a single species to determine the specific gravity relations within that species. It has been applied to a few of the properties of some of the more important species which are used for structural timbers where there was a rather large number of test pieces and a considerable range in specific gravity.

DETERMINATION OF SPECIFIC GRAVITY.

Specific gravity of wood, as used herein, is based on the volume of the specimens when tested (green or air-dry) and their weight when in an oven-dry condition; that is, it is the ratio of the weight of the specimen of wood, *oven-dry*, to the weight of a volume of water equal to the *volume of the specimen at the time of test*. Because of the shrinkage which takes place in wood when it is dried, this figure is not the true specific gravity of a piece of oven-dry wood. The method, however, is easily applied to each specimen tested, and is the standard method of the Forest Service for the determination of a specific-gravity figure for use in studying the properties of wood.

MOISTURE CONTENT OF TEST SPECIMENS.

Both green and air-dry specimens were used in the tests, and the relations between specific gravity and strength were determined separately for green and air-dry wood. Variations in the moisture content of wood have no effect on its mechanical properties so long as the wood is thoroughly green; they have considerable influence on these properties, however, as soon as the wood becomes air-dry, or partially air-dry. Accurate comparisons can not be made between the properties of two lots of air-dry specimens unless they were tested at the same moisture content or adjustments made in the strength figures for difference in moisture content.

The moisture content of the air-dry material at the time of test varied from 8 to 18 per cent. Modulus of rupture and maximum strength in compression parallel to the grain were adjusted to a moisture content of 12 per cent before determinations of the relation of these properties to the specific gravity was made. This adjustment was possible because the laws governing the variation of these properties with varying moisture content are fairly well established. However, in the case of the other strength functions their variation with varying moisture content has not been studied in detail and no such adjustment is possible with any very great degree of accuracy. Consequently, the actual moisture content values as obtained from tests have been used in the determination of the relation of these properties to specific gravity.

THE EQUATIONS.

Table 1 and figures 1 to 4 give equations which represent the average relations between specific gravity and each of the mechanical properties. All the "species-locality" averages available on any particular property were considered in deriving the equations for that property. The number of "species-locality" averages from which an equation is derived varies from 84 to 178. This variation is due to the fact that several of the tests were not used in some of the earlier testing work and to the fact that tests have not yet been completed on air-dry material for all of the "species-localities" listed.

Table 1 gives first the equations for shrinkage and for each of the strength properties of green and air-dry wood in terms of the specific gravity. These equations, as explained in the appendix, are reduced to a simple form; and the powers of gravity used are such that the equations may be solved by arithmetical operations and without the use of higher mathematics. However, to simplify even further the use of the equations, figures 1 to 4 have been prepared for their solution. Each of the curves shown in these diagrams represents the equation connecting specific gravity and one of the properties of wood. The curves representing the equations for radial, tangential, and volumetric shrinkage appear in figure 1(a). In each of the other figures, 1(b) to 4(d), appear two curves for some one mechanical property. One of these curves is for green and the other for air-dry material. If the specific gravity is known, the equation value for any one or all of the properties of the wood in question may be readily determined from the curves without computation.

The second portion of Table 1 gives what may be termed a measure of the accuracy of the respective equations. It is not to be expected that all the "species-locality" averages will satisfy the equation exactly or even very closely. Some of the properties are more erratic than others, so that one "species-locality" may far exceed

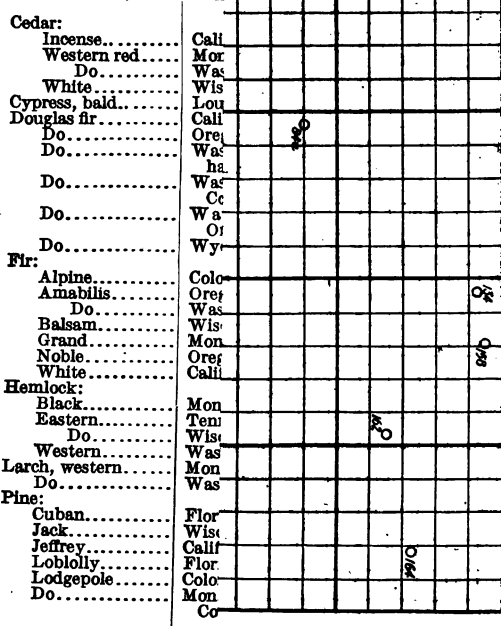
the equation values and another "species-locality" fall far below them.

In figure 5 are plotted the curves of the equation for modulus of rupture in static bending in green material, $M=18500 \sqrt[3]{g^5}$, and of the equation for the same property in air-dry material, $M=26200 \sqrt[3]{g^5}$. In order to give a graphical idea as to the reliability of these equations, the specific gravity and the modulus of rupture of each "species-locality" have been plotted as a point. The reference number placed near each plotted point is assigned to the "species-locality" in the order of its respective specific gravity as determined from compression parallel to grain specimens of green wood. In figures 6, 7, and 8 the data are given for the curves on shrinkage in volume from green to oven-dry condition, maximum crushing strength in compression parallel to grain, and fiber strength at elastic limit in compression perpendicular to grain.

Under each property is listed in this second portion of Table 1, for both green and air-dry conditions, those percentages of the equation value above which were one-tenth of the "species-localities." Similarly, there are listed those percentages above which were one-fourth of the "species-localities," those below which were one-fourth, and those below which were one-tenth. For instance, in static bending (green), one-tenth of the "species-localities" tested had a modulus of rupture of more than 114 per cent of what the specific gravity equation indicated they should have had; one-fourth of them had a modulus of rupture greater than 108 per cent of the equation value; one-fourth of them less than 91 per cent of the equation value; and the lowest one-tenth had a modulus of rupture less than 84 per cent of what the equation indicated they should have had. It follows from these figures that one-half of the "species-localities" had a modulus of rupture of between 91 per cent and 108 per cent of the value given by the equation, and that the other one-half were evenly divided between those that were more than 108 per cent and those that were less than 91 per cent.

The third portion of Table 1 gives the actual value of each property for each "species-locality" as determined by the tests, expressed as a percentage of the value computed from the specific gravity by the use of the equation at the head of the column. For instance, it is found from the table that air-dry Biltmore ash has a modulus of rupture 98 per cent as great as that of the average wood of its specific gravity, the modulus of rupture of the average wood of this specific gravity being the figure given by the equation. These percentages are given for both green and air-dry wood.

00 21



the equation value them.

In figure 5 are rupture in static the equation for the In order to give equations, the species "species-locality" ber placed near each in the order of compression parallel 6, 7, and 8 the data from green to over compression parallel compression perpendicular

Under each profile both green and air value above which locally, there are lists of the "species-locality" those below which (green), one-tenth rupture of more than

indicated they show rupture greater than of them less than one-tenth had a maximum equation indicated figures that one-half rupture of between the equation, and those that were more 91 per cent.

The third portion for each "species-locality" percentage of the use of the equation found from the rupture 98 per cent gravity, the modulus gravity being the figure given for both green

Species	Value	Species	Value	Species	Value
Wisconsin	53	Willow	100	Louisiana, Parish	100
Illinois	165	Yellow	122	Arkansas	122
Tennessee	68	Do	105	Wisconsin	105
Florida	147	Ossage orange	164	Indiana	164
Illinois	76	Poplar, yellow (tulip tree)	35	Tennessee	35
Missouri	54	Rhododendron, great	85	Do	85
Illinois	90	Sassafras	51	Do	51
Wisconsin	78	Serviceberry	156	Do	156
Do	146	Silverbell tree	49	Do	49
Mississippi	135	Sourwood	89	Do	89
Do	154	Sumac, staghorn	61	Wisconsin	61
Mississippi	139	Sycamore	63	Indiana	63
Illinois	144	Do	65	Tennessee	65
Illinois	159	Umbrella, Fraser	45	Do	45
West Virginia	155	Willow			
Mississippi	112	Black	11	Wisconsin	11
Do	143	Western black	43a	Oregon	43a
Illinois	157	Witch hazel	114	Tennessee	114
Illinois	160				
West Virginia	161				

CONIFERS.

Species	Value	Species	Value	Species	Value
Florida	26	Pine—Continued		Montana, Granite	41a
Illinois	2	Lodgepole		County	
Washington	10	Do		Montana, Jefferson	40a
Wisconsin	1	Do		County	
Illinois	62	Do		Wyoming	34
Florida	45a	Longleaf		Florida	123
Illinois	67a	Do		Louisiana, Lake	113
Washington, Che-	40a	Do		Charles	
allis County		Do		Louisiana, Tangipahoa Parish	96
Washington, Lewis	75	Do		Mississippi	95
County		Norway		Wisconsin	57
Washington and	67	Pitch		Tennessee	71
regon	48	Pond		Florida	86
oming		Shortleaf		Arkansas	77
Colorado	4	Sugar		California	22
Illinois	39	Table Mountain		Tennessee	82
Washington	18	Western white		Montana	42
Wisconsin	14	Western yellow		Arizona	19
Illinois	36	Western		California	37
Illinois	16	Do		Colorado	41
Florida	17	Do		Montana	32
Tennessee	47	White		Wisconsin	25
Tennessee	52	Redwood		California, Albi	28
Wisconsin	15	Do		California, Korb	13
Washington	50	Spruce			
Illinois	84	Engelmann		Colorado, Grand	8
Illinois	64	Do		County	
Idaho	127	Do		Colorado, San	3
Wisconsin	43	Red		Miguel County	
Idaho	33	Do		New Hampshire	44
Idaho	88	White		Tennessee	20
Idaho	31	Do		New Hampshire	7
Tennessee	35a	Tamarack		Wisconsin	38
County		Yew, western		Do	81
				Washington	134

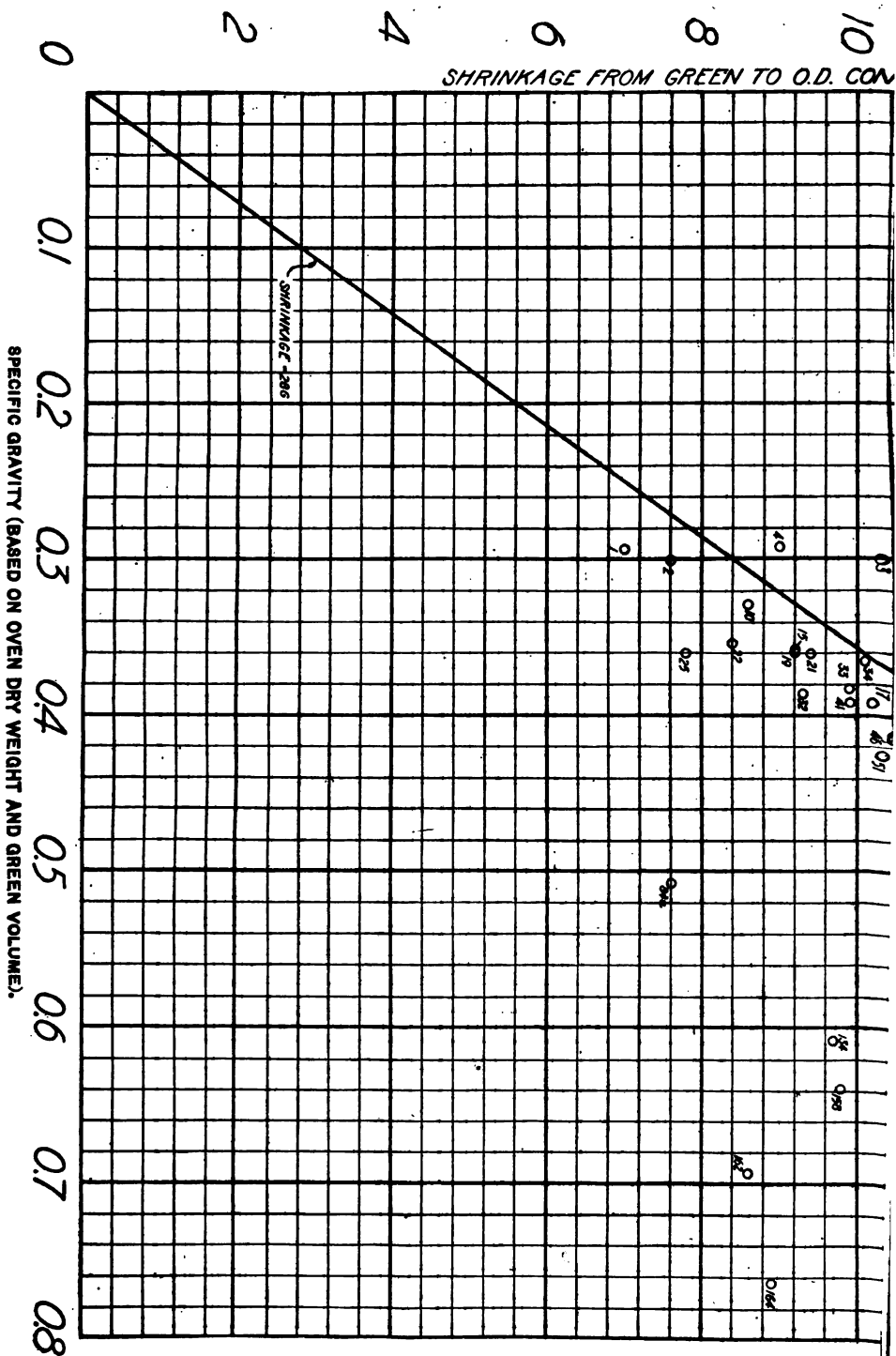


FIG. 6.—Relation of shrinkage from green

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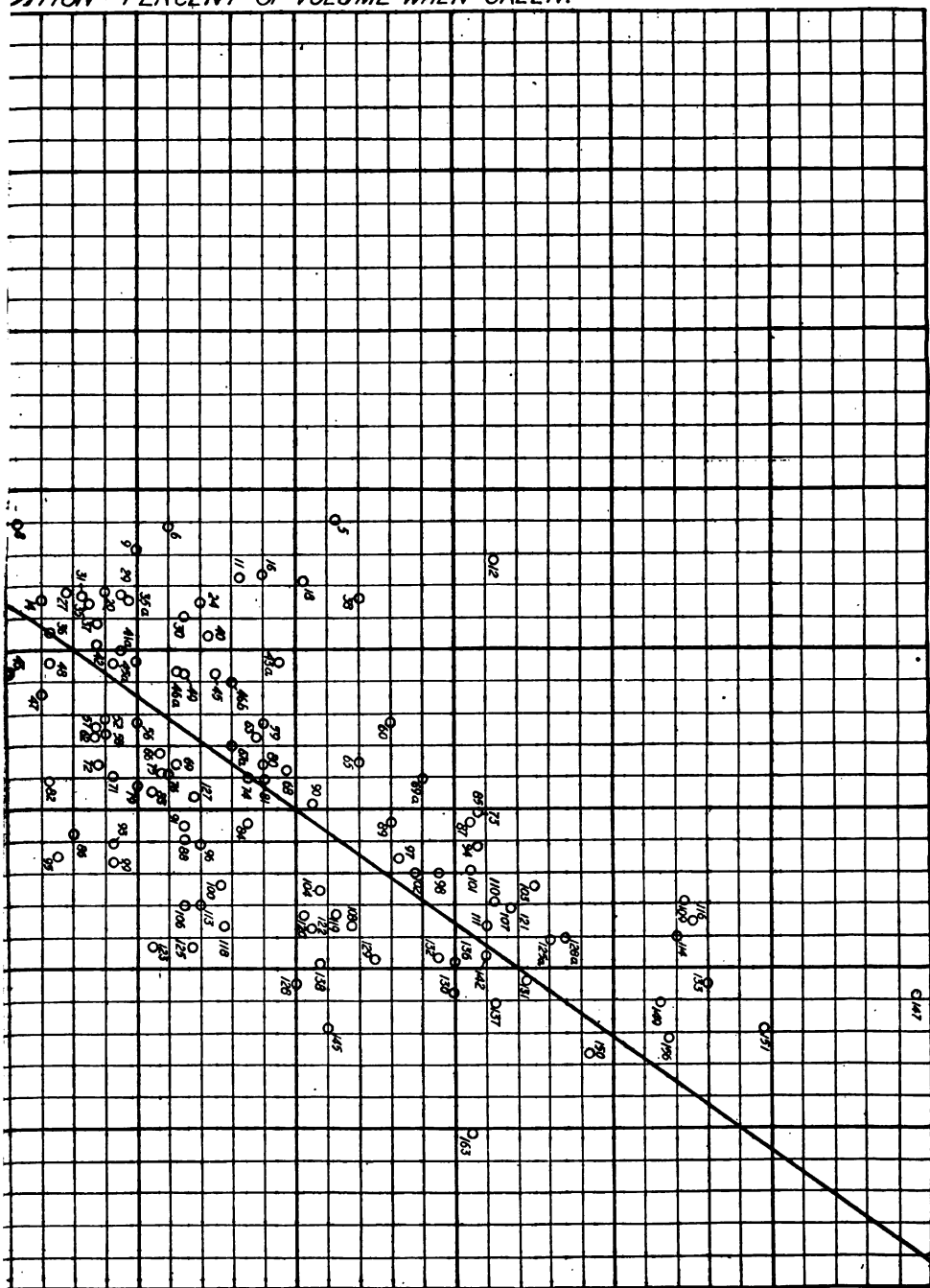
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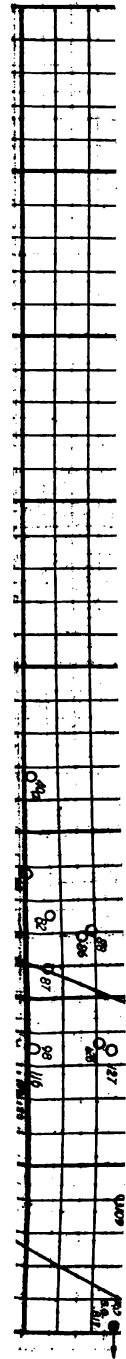
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ADDITION - PERCENT OF VOLUME WHEN GREEN.



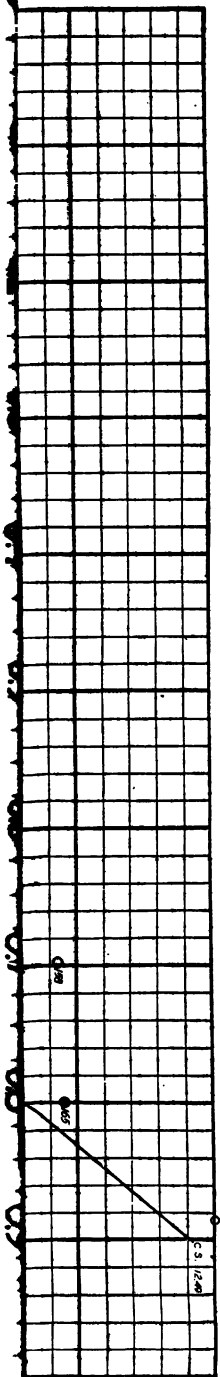
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PERPEN.



section per per

11

10



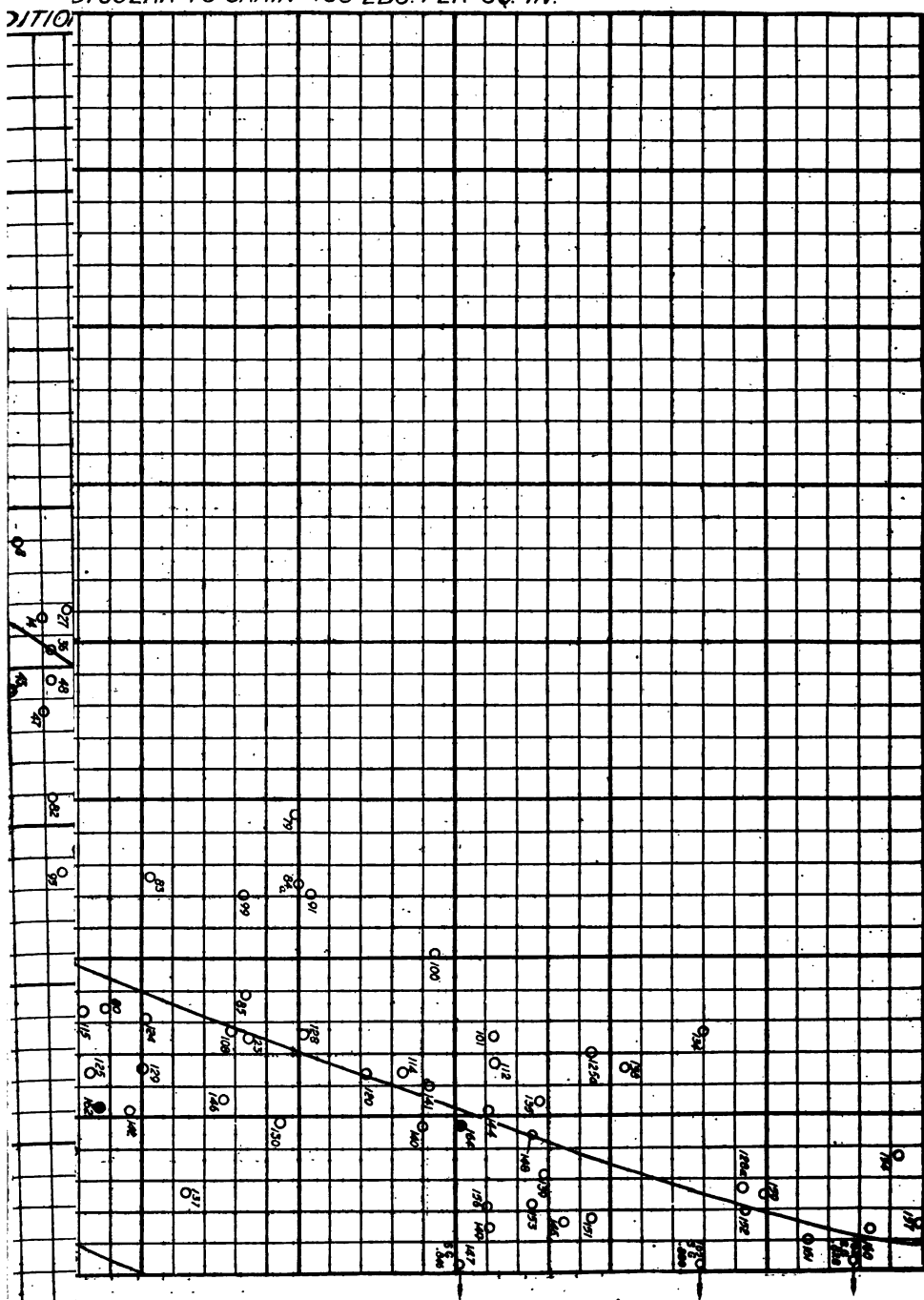
SPECIFIC GRAVITY (BASED ON OVEN DRY WEIGHT AND VOLUME AS TESTED).

30

25

20

PERPENDICULAR TO GRAIN-100 LBS. PER SQ. IN.



perpendicular to grain to specific gravity.

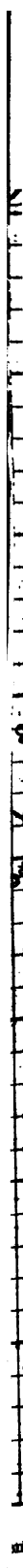
ASTATIC GRAVITY

1.3

0.0

3

6



APPLICATION OF THE EQUATIONS.

Additional data may possibly necessitate the making of some slight changes in the equations given in Table 1 and the diagrams. However, for comparing species and for determining the best utilization of timber, the value of the equations as they are now is not affected by this possibility. It is to be expected that among a large number of species of widely different structure many will be found which do not satisfy very accurately the average equations connecting the various properties with specific gravity. It is often this variation from an average relation which determines the usefulness of a species for a special purpose.

As an example of the use to which the table and diagrams may be put, suppose it is desired to obtain the strength in compression parallel to the grain of a piece of green hemlock (eastern) grown in the southern Appalachian region. Its specific gravity may be determined by any one of several means which may readily be devised, and we will say that it is found to be 0.38. In the table, the "species-locality" which is probably most nearly representative of the region in question is the eastern hemlock from Tennessee, and of this the maximum crushing strength is 29 per cent above the average for woods of the same specific gravity. To find what an average wood of a specific gravity of 0.38 will stand in compression parallel to the grain, we solve the equation $C = 6,900 \times 0.38$, or turn to figure 1 and read from the curve a maximum crushing strength of about 2,600 pounds per square inch. But since the compressive strength of the Tennessee hemlock was 29 per cent high, it is reasonable to expect that the timber in question will also run about 29 per cent high, or that the value would be about 3,300 or 3,400 pounds per square inch ($2,600 \times 1.29 = 3,354$). Any of the other properties of the hemlock under consideration may be estimated in a similar manner.

Again, suppose it is desired to obtain a wood for a use which requires that it be very strong for its weight in its ability to resist a splitting force. Tension perpendicular to grain is the best measure of this. By looking down the column, "Tension, surface of failure radial," it is found that in ability to resist such a force, yellow buckeye is 17 per cent stronger when green and 120 per cent stronger when air-dry than is the average wood of the same specific gravity. It would appear at first that yellow buckeye is the most desirable wood for the purpose, but there is another consideration to be taken into account. Tension perpendicular to the grain varies with the square of the specific gravity; and it must be remembered that those properties (such as tension perpendicular to grain, hardness, work values, and compression perpendicular to the grain) which vary with the higher powers of specific gravity show a large increase in strength

with a comparatively small increase in specific gravity. For instance, a wood with twice the specific gravity of another would be expected to have four times as much strength in tension. Yellow buckeye is a very light wood and woods of more than double its specific gravity may easily be found. Such woods, even though they may run somewhat less in tension strength than the average wood of their weight, may have a tension strength considerably in excess of that of yellow buckeye. Thus, the red oaks, having a specific gravity of about twice that of yellow buckeye, are several times as strong in tension perpendicular to the grain, although they are very little above the average wood of their weight in this respect.

It may be seen from these examples that in comparing different timbers or species, in estimating their various properties, and in finding species with exceptional strength in some properties which may render them valuable for special uses, a knowledge of the specific-gravity strength relations is a valuable aid. It must be borne in mind, however, that such equations can never take the place of tests of species whose properties are unknown. If any particular mechanical property is known, the specific gravity may be approximated and the other properties estimated; even the properties of woods upon which no test data are available can be estimated with a fair degree of accuracy from the results of specific gravity determinations. Nevertheless, it is apparent from a study of the table and diagrams that no one kind of test can replace a complete series of tests.

APPENDIX.

METHOD OF DERIVING EQUATIONS.

In plotting the various points to a natural scale (i. e., the shrinkage or a given mechanical property vs. specific gravity) it was found that in many cases they arranged themselves in the form of a curve, or if their trend was along a straight line, this line would not pass through the origin. Assuming that the function should pass through the origin, i. e., that a piece of wood of zero weight or specific gravity should have zero strength, it was found that in practically every case a curve of the form $f=pG^n$ (where f is the strength value, G the specific gravity, and p and n are constants) would fit the points quite well. This equation is the general equation of the parabola of the n th degree passing through the origin.

In order to simplify the determination of the proper values for the constants p and n the equation was transformed into the logarithmic form, $\log f = \log p + n \log G$. This equation represents a straight line having its slope equal to n and its intercept on the y axis equal to $\log p$. Consequently, to find the constants p and n it is only necessary to plot $\log f$ against $\log G$ on ordinary cross-section paper and find the straight line which best averages the points; then n and $\log p$ are determined from the slope and intercept of this line.

To find the straight line which best averages the points in the logarithmic plot the following plan was adopted:

By successive trials the parallel lines BB and CC (see fig. 9) were so located that 25 per cent of the points were above BB and 25 per cent were below CC and at the same time the vertical distance between the two was a minimum. Two lines (not shown on the figure) were then drawn as follows: Both parallel to BB and CC, one bisecting the distance between them and the other in such a position that 50 per cent of the points were on each side of it. AA was then drawn midway between these two lines and assumed to be the line which best averages the points and best represents the relation between specific gravity and the strength property in question. This method, as can readily be seen, is very likely to produce values of n such that the resulting equations can not be handled without the use of logarithms. As the slope of the lines could in most cases be varied through a considerable angle without appreciably affecting the distance between the lines BB and CC, the slope was so taken that n would be a fraction with the denominator 1, 2, 3, or 4. The solution of the equation is then possible by using the rules for the extraction of square and cube roots. Whenever it happened that more than one direction of the lines BB and CC fulfilled the conditions outlined above, preference was given to that slope which would simplify the form of the equation. The constant p was changed at the same time, so that the new line A'A' passed as nearly through the center of gravity of the points as possible.

The analytical process known as the "method of least squares" can be applied to determining the mathematical relations between two properties of a substance as ascertained from experimental results. This method was used in one or two instances to determine the specific gravity strength relations; but it was found that the long and refined computations essential to the application of this method to so large a number of tests was not justified by the added accuracy of the final determinations. Especially is this true since it is desirable to obtain n to the nearest 0.125 only, and since undue refinement in the value of the constant p is unnecessary in view of the fact that there is a considerable variation of actual results from the values given by any equation which may be derived.

TABLE 1.—Equations and variations—Specific gravity, shrinkage, and strength relations based on tests of small clear pieces, green and air-dry.

Species and locality.	Reference number.	Specific gravity, oven-dry, based on volume at time of test.	Per cent.	Moisture content.	Shrinkage from green to oven-dry condition.	Static bending.										Impact bending, 50-pound hammer.				Compression parallel to grain.				Hardness: Load required to embed a 0.44-inch ball one-half its diameter.			Shear.		Cleavage.		Tension.																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																											
						In volume.	Radial.	Tangential.	Fiber stress at elastic limit.	Lbs. per sq. in.	Lbs. per sq. in.	Modulus of elasticity.	Inch lbs. per cu. in.	Work to elastic limit.	Work to maximum load.	Inch lbs. per cu. in.	Total work.	Fiber stress at elastic limit.	Lbs. per sq. in.	1,000s of lbs. per sq. in.	Inch lbs. per cu. in.	Inches.	Height of drop causing complete failure.	Fiber stress at elastic limit.	Lbs. per sq. in.	Maximum crushing strength.	Modulus of elasticity.	End surface.	Radial surface.	Tangential surface.	Surface of failure radial.	Surface of failure tangential.	Lbs.	Surface of failure radial.	Surface of failure tangential.	Lbs.	Surface of failure radial.	Surface of failure tangential.	Lbs. per sq. in.	Lbs. per sq. in.																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
Per cent of dimensions when green.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent.	Per cent

I.—EQUATIONS FOR SHRINKAGE AND FOR EACH OF THE STRENGTH PROPERTIES OF GREEN AND AIR-DRY WOOD IN TERMS OF SPECIFIC GRAVITY.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	
Green.....							$F = 19000 \sqrt{G}$	$M = 26200 \sqrt{G}$	$E = 3000 G$	$W = 9.0 G$	$W = 38.9 G$	$W = 148.0 G$	$F = 35000 \sqrt{G}$	$E = 3550 G$	$W = 15.1 G$	$H = 111 G$	$F = 11000 \sqrt{G}$	$C = 12000 G$	$E = 3500 G$	$F = 5200 \sqrt{G}$	$H = 4800 \sqrt{G}$	$H = 3600 \sqrt{G}$	$H = 3800 \sqrt{G}$	$S = 3630 \sqrt{G}$	$S = 2550 \sqrt{G}$	$S = 2750 \sqrt{G}$	$C = 1100 G$	$C = 1300 G$	$T = 2100 G$	$T = 2400 G$
	Green to oven-dry.....						$F = 10300 \sqrt{G}$	$M = 18500 \sqrt{G}$	$E = 2800 G$	$W = 3.51 G$	$W = 42.7 G$	$W = 186.0 G$	$F = 23500 \sqrt{G}$	$E = 3000 G$	$W = 15.1 G$	$H = 140 G$	$F = 68.0 \sqrt{G}$	$C = 6900 G$	$E = 2860 G$	$F = 2900 \sqrt{G}$	$H = 3700 \sqrt{G}$	$H = 3300 \sqrt{G}$	$H = 3300 \sqrt{G}$	$S = 2550 \sqrt{G}$	$S = 2550 \sqrt{G}$	$S = 2750 \sqrt{G}$	$C = 1070 G$	$C = 1300 G$	$T = 1960 G$	$T = 2300 G$
		Air-dry.....						$F = 170 G$	$M = 170 G$	$E = 170 G$	$W = 170 G$	$W = 170 G$	$W = 170 G$	$F = 170 G$	$E = 170 G$	$W = 170 G$	$H = 170 G$	$F = 170 G$	$C = 170 G$	$E = 170 G$	$F = 170 G$	$H = 170 G$	$H = 170 G$	$H = 170 G$	$S = 170 G$	$S = 170 G$	$S = 170 G$	$C = 170 G$	$C = 170 G$	$T = 170 G$

III.—MEASURE OF ACCURACY OF RESPECTIVE EQUATIONS.

[illegible]

III.—ACTUAL VALUE OF EACH PROPERTY FOR EACH "SPECIES-LOCALITY" AS DETERMINED BY TESTS—EXPRESSED IN PERCENTAGE OF EQUATION VALUE.

[illegible]

TABLE 1.—Equations and variations—specific gravity, shrinkage, and strength relations based on tests of small clear pieces, green and air-dry—Con.

Species and locality.	Reference number.	Specific gravity, oven-dry, based on volume at time of test.	Per cent.	Moisture content.	Shrinkage from green to oven-dry condition.			Static bending.										Impact bending, 50-pound hammer.					Compression parallel to grain.				Hardness: load required to embed a 0.444-inch ball one-half its diameter.	Shear.		Cleavage.		Tension.	
					In volume.	Radial.	Tangential.	Fiber stress at elastic limit.	Lbs. per sq. in.	Lbs. per sq. in.	Modulus of elasticity.	Work to elastic limit.	Inch lbs. per cu. in.	Work to maximum load.	Total work.	Fiber stress at elastic limit.	Lbs. per sq. in.	1,000s of lbs. per sq. in.	Modulus of elasticity.	Height of drop causing complete failure.	Fiber stress at elastic limit.	Maximum crushing strength.	Lbs. per sq. in.	1,000s of lbs. per sq. in.	Compression perpendicular to grain, fiber stress at elastic limit.	End surface.		Radial surface.	Tangential surface.	Lbs. per sq. in.	Surface of failure radial.	Surface of failure tangential.	Lbs. per sq. in.

III.—ACTUAL VALUE OF EACH PROPERTY FOR EACH "SPECIES-LOCALITY" AS DETERMINED BY TESTS—EXPRESSED IN PERCENTAGE OF EQUATION VALUE—Continued.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	
Ash, green (Louisiana):																														
Green.....	93						69	110	102	94	94	77	112	90	137	86	108	113	101	117	107	105	106	118	102	119	99	119		
Air-dry.....							98	106	97	104	104	97	91	95	90	90	91	92	96	95	124	121	107	111	93	90	100	111		
Ash, pumpkin (Missouri):																														
Green.....	100						128	118	110	139	104	92	103	98	102	92	126	115	101	139	114	118	124	120	109	103	98	100		
Air-dry.....							100	105	99	100	106	80	103	108	108	83	105	97	104	135	125	130	112	135	120	159	126	114		
Ash, white (Missouri):																														
Green.....	79						107	101	86	130	94	69	90	82	101	92	103	100	80	180	121	119	112	124	112	124	121	125	101	
Air-dry.....							77	88	81	81	67	60	98	93	117	76	85	89	66	172	122	114	107	134	105	174	114	182	98	

[illegible]

TABLE 1.—Equations and variations—specific gravity, shrinkage, and strength relations based on tests of small clear pieces, green and air-dry—Con.

Species and locality.	Reference number.	Specific gravity, oven-dry, based on volume at time of test.	Per cent.	Moisture content.	Shrinkage from green to oven-dry condition.	Static bending.										Impact bending, 50-pound hammer.				Compression parallel to grain.				Hardness: load required to embed a 0.444-inch ball one-half its diameter.	Shear.		Cleavage.	Tension.	
						In volume.	Radial.	Tangential.	Fiber stress at elastic limit.	Lbs. per sq. in.	Lbs. per sq. in.	Modulus of rupture.	Modulus of elasticity.	Work to elastic limit.	Inch lbs. per cu. in.	Work to maximum load.	Inch lbs. per cu. in.	Total work.	Fiber stress at elastic limit.	Lbs. per sq. in.	Lbs. per sq. in.	Modulus of elasticity.	Maximum crushing strength.		Modulus of elasticity.	End surface.		Radial surface.	Tangential surface.

III.—ACTUAL VALUE OF EACH PROPERTY FOR EACH "SPECIES-LOCALITY" AS DETERMINED BY TESTS—EXPRESSED IN PERCENTAGE OF EQUATION VALUE—Continued.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
Buckeye, yellow (Tennessee):																													
Green.....	9			127	113	141	99	100	115	100	109	92	105	112	121	112	99	91	106	88	121	110	108	122	112	119	139	117	142
Air-dry.....							124	92	113	174	110	100	121	107	175	90	128	87	138	94	96	110	107	110	107	128	174	220	182
Buckthorn, cascara (Oregon):																													
Green.....	84a			54	68	55	77	82	50	117	125	185	85	76	91	157	67	96	70	114	90	112	105	118	95	83	81	101	85
Air-dry.....																													
Butternut (Tennes- see):																													
Green.....	27			109	87	105	91	95	104	94	145	162	119	118	144	148	95	90	85	94	106	108	119	106	119	139	157	167	169
Air-dry.....							103	81	104	132	156	266	109	122	121	151	128	92	133	117	104	105	119	118	119	102	110	114	151

Butternut (Wisconsin):	21	93	107	95	108	113	110	130	149	177	107	110	123	121	115	106	123	90	112	121	121	114	115	154	145	159	159
Green:					144	111	111	210	117		130	117	183	130		117	92	130	97	106	110	131	184	151	135	116	125
Air-dry:																											
Chinquapin, western (Oregon):	466	112	116	105	119	110	95	169	123	106	110	100	128	126	85	105	128	125	135	137	114	119	194	108	110	137	121
Green:																											
Air-dry:																											
Cherry, black (Pennsylvania):	72	87	82	89	103	111	111	102	135	125	110	105	123	107	111	109	114	86	117	121	112	115	117	119	128	114	130
Green:																											
Air-dry:																											
Cherry, wild red (Tennessee):	24	124	81	168	99	96	115	100	110	137	98	107	105	118	96	87	103	90	110	108	112	93	101	109	106	104	106
Green:																											
Air-dry:																											
Chestnut (Maryland):	46	90	86	97	97	100	93	110	104	114	106	110	108	102	100	97	86	105	108	93	100	117	100	128	125	149	132
Green:																											
Air-dry:																											
Chestnut (Tennessee):	40	118	92	103	90	93	94	100	106	103	104	98	124	107	91	83	86	107	116	105	110	103	89	130	111	123	112
Green:																											
Air-dry:																											
Cottonwood, black (Washington):	6	109	120	161	117	111	135	121	118	149	119	124	144	139	111	99	126	93	101	103	106	100	105	125	146	117	132
Green:																											
Air-dry:																											
Cucumber tree (Tennessee):	59	109	124	118	112	110	140	94	119	101	109	127	100	111	114	108	133	90	93	93	90	103	117	110	112	107	106
Green:																											
Air-dry:																											
Dogwood, flowering (Tennessee):	161	111	116	104	82	84	74	77	121	94	52	43	56	99		83		95	104	118	115	102	103				
Green:																											
Air-dry:																											
Dogwood, western (Oregon):	125a	106	116	97	80	83	75	77	117	89	82	87	71	119	66	91	93	106	112	110	106	98	105	78	86	104	102
Green:																											
Air-dry:																											
Elder, pale (Oregon):	69a	116	99	115	87	94	78	96	97	149	85	88	65	120	96	96	111	99	124	135	135	115	105	139	96	126	108
Green:																											
Air-dry:																											
Elm, cork (Wisconsin, Marathon County):	128																										
Green:																											
Air-dry:																											

Hickory, nutmeg (Mississippi):	112	97	101	92	96	169	149	115	88	138	130	111	104	89	125	90	86
Green:	88	110	98	72	172	89	109	110
Air-dry:
Hickory, pignut (Mississippi):	148	112	114	106	102	145	121	114	88	125	150	92	113	82	114	79	74
Green:	100	111	115	79	114	114	113	112	110	107	98	100	102
Air-dry:
Hickory, pignut (Ohio):	157	110	110	93	108	144	140	105	72	138	182	102	105	90	108	98	113
Green:	87	106	110	67	101	122	107	123	87	152	92	102	125	115
Air-dry:
Hickory, pignut (Pennsylvania):	160	99	103	96	86	182	138	112	97	112	149	105	105	100	98	87	87
Green:	91	103	100	69	137	139	103	104	90	100	99	100	85	78
Air-dry:
Hickory, pignut (West Virginia):	161	92	104	104	69	156	132	131	95	146	110	87	104	104	94	86	87
Green:	94	94	103	77	128	115	92	93	94	90	85
Air-dry:
Hickory, shagbark (Mississippi):	140	112	114	107	102	106	130	111	95	115	97	115	121	108	121	90	91
Green:	94	103	102	81	97	128	93	100	85	113	99	92	122	112
Air-dry:
Hickory, shagbark (Ohio):	152	91	103	83	86	190	149	92	84	88	174	73	98	81	96	94	99
Green:	76	107	95	51	137	97	119	96	96	81
Air-dry:
Hickory, shagbark (Pennsylvania):	143	104	100	90	121	74	146	76	103	59	87
Green:	120	115	93	163	94	95	94
Air-dry:
Hickory, shagbark (West Virginia):	153	101	101	107	81	100	121	114	100	110	98	95	103	105	88	84	82
Green:	98	106	108	77	114	101	106	87	106	103	86	94	93
Air-dry:
Hickory, water (Mississippi):	141	103	103	99	92	111	98	104	93	102	101	90	112	111	117	102	101
Green:	105	111	111	93	117	110	107	106	109	100	80
Air-dry:
Holly, American (Tennessee):	87	114	94	111
Green:	81	72	69	95	77	40	85	77	104	76	76	76	73	62	100	114	128
Air-dry:	100	112	132	95
Hornbeam (Tennessee):	149	107	135	89	79	83	74	74	80	76	69	82	75	71	76	62	132
Green:	88	56	74
Air-dry:	94	72
Laurel, mountain (Tennessee):	145	81	95	84
Green:	104	85	60	154	79	53	76	59	86	57	101	108	112	116
Air-dry:	88	62	66	105	46	30	75	71	71	79	72	65	62	85	112	113

TABLE 1.—Equations and variations—specific gravity, shrinkage, and strength relations based on tests of small clear pieces, green and air-dry—Con.

Species and locality.	Reference number.	Specific gravity, oven-dry, based on volume at time of test.	Per cent.	Moisture content.	Shrinkage from green to oven-dry condition.			Static bending.						Impact bending, 50-pound hammer.						Compression parallel to grain.				Hardness: load required to embed a 0.444-inch ball one-half its diameter.	Shear.		Cleavage.		Tension.																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																					
					In volume.	Radial.	Tangential.	Lbs. per sq. in.	Modulus of rupture.	1,000s of lbs. per sq. in.	Inch lbs. per cu. in.	Work to elastic limit.	Inch lbs. per cu. in.	Work to maximum load.	Total work.	Lbs. per sq. in.	Fiber stress at elastic limit.	Modulus of elasticity.	Inch lbs. per cu. in.	Work to elastic limit.	Height of drop causing complete failure.	Lbs. per sq. in.	Maximum crushing strength.		1,000s of lbs. per sq. in.	Lbs. per sq. in.	Compression perpendicular to grain.	End surface.	Radial surface.	Tangential surface.	Lbs. per sq. in.	Surface of failure radial.	Lbs. per sq. in.	Surface of failure tangential.	Lbs. per sq. in.	Surface of failure radial.	Lbs. per sq. in.	Surface of failure tangential.																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																												
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III.—ACTUAL VALUE OF EACH PROPERTY FOR EACH "SPECIES-LOCALITY" AS DETERMINED BY TESTS—EXPRESSED IN PERCENTAGE OF EQUATION VALUE—Continued.

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[illegible]

Cedar, white (Wisconsin); Green; Air-dry	85	75	95	115	106	87	196	156	132	105	90	121	128	97	98	90	151	110	88	126	115	156	128	149	121
Cypress, bald (Louisiana); Green; Air-dry	91	89	78	117	105	123	135	59	71	94	106	88	81	141	127	134	115	77	67	67	95	84	72	69	61
Douglas fir (California); Green; Air-dry	102	118	102	126	114	133	128	85	72	113	130	110	92	127	123	182	114	101	98	101	102	95	61	53	62
Douglas fir (Oregon); Green; Air-dry	101	129	97	123	111	144	105	76	76	107	127	93	88	132	128	180	104	81	83	90	93	89	39	26	43
Douglas fir (Cherokee County, Washington); Green; Air-dry	108	111	105	122	111	133	117	81	86	107	131	97	85	127	119	167	121	95	92	97	117	102	66	69	58
Douglas fir (Lewis County, Washington); Green; Air-dry	93	110	103	130	110	136	121	71	83	101	126	83	83	140	126	165	101	74	77	83	96	89	62	58	49
Douglas fir (Washington and Oregon); Green; Air-dry				133	118	138									127										
Douglas fir (Wyoming); Green; Air-dry	95	92	93	107	100	116	92	90	72	103	119	94	74	105	101	120	111	77	85	88	98	91	62	50	
Fir, alpine (Colorado); Green; Air-dry	110	85	137	97	102	109	110	104	87	97	105	110	67	108	97	100	154	125	100	117	107	112	121	108	
Fir, amabilis (Oregon); Green; Air-dry				103	111	91	184	81	128	71	96	71	106	123	111	95	125	96	90	122	102	113	101	90	
Fir, amabilis (Frischman's Washington); Green; Air-dry	140	135	168	122	110	139	130	108	106	122	143	118	121	130	110	153	108	104	94	108	105	98	94	76	104
Fir, balsam (Wisconsin); Green; Air-dry	105	88	116	112	102	113	129	96	76	112	114	132	99	129	104	132	81	87	94	104	99	94	96	90	74

TABLE 1.—Equations and variations—specific gravity, shrinkage, and strength relations based on tests of small clear pieces, green and air-dry—Con.

Reference number.	Specific gravity, oven-dry, based on volume at time of test.	Per cent.	Moisture content.	Shrinkage from green to oven-dry condition.			Static bending.								Impact bending, 50-pound hammer.				Compression parallel to grain.				Hardness: load required to embed a 0.444-inch ball one-half its diameter.	Shear.		Cleavage.		Tension.																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																			
				In volume.	Radial.	Tangential.	Lbs. per sq. in.	Modulus of rupture.	1,000s of lbs. per sq. in.	Inch lbs. per cu. in.	Work to elastic limit.	Work to maximum load.	Inch lbs. per cu. in.	Total work.	Fiber stress at elastic limit.	1,000s of lbs. per sq. in.	Modulus of elasticity.	Inch lbs. per cu. in.	Height of drop causing complete failure.	Fiber stress at elastic limit.	Lbs. per sq. in.	Maximum crushing strength.		Modulus of elasticity.	Lbs. per sq. in.	Compression perpendicular to grain, fiber stress at elastic limit.	End surface.	Radial surface.	Tangential surface.	Surface of failure	Surface of failure radial.	Surface of failure tangential.	Lbs. per sq. in.	Surface of failure	Lbs. per sq. in.	Surface of failure tangential.	Lbs. per sq. in.																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																										

III.—ACTUAL VALUE OF EACH PROPERTY FOR EACH "SPECIES-LOCALITY" AS DETERMINED BY TESTS—EXPRESSED IN PERCENTAGE OF EQUATION VALUE—Continued.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30		
CONIFERS—cont'd.																															
Fir, grand (Montana):																															
Green.....	36			101	93	107	106	133	104	94	120	120	126	127	139	125	117	168	100	106	95	104	111	105	103	85	90	74			
Air-dry.....							108	104	146	96	142	323	145	130	166	169	101	79	113	113	98	142	101	97	328	66	45	52			
Fir, noble (Oregon):																															
Green.....	16			137	147	143	119	143	117	112	135	120	128	133	111	130	112	171	111	85	76	83	105	101	76	63	71				
Air-dry.....																															
Fir, white (California):																															
Green.....	17			93	102	113	135	116	125	169	94	123	114	126	121	105	144	116	132	146	106	100	105	113	103	106	119	94	103		
Air-dry.....							119	108	127	137	92	113	82	93	93	91	139	115	129	118	150	121	119	98	109	106	104	75	90		

RELATION OF SHRINKAGE, ETC., TO SPECIFIC GRAVITY.

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TABLE 1.—Equations and variations—specific gravity, shrinkage, and strength relations based on tests of small clear pieces, green and air-dry—Con.

Species and locality.	Reference number.	Specific gravity, oven-dry, based on volume at time of test.	Per cent.	Moisture content.	Shrinkage from green to oven-dry condition.			Static bending.										Impact bending, 50-pound hammer.				Compression parallel to grain.				Hardness: load required to embed a 0.444-inch ball one-half its diameter.	Shear.		Cleavage.		Tension.	
					In volume.	Radial.	Tangential.	Lbs. per sq. in.	Lbs. per sq. in.	Modulus of rupture.	1,000s of lbs. per sq. in.	Inch lbs. per cu. in.	Work to elastic limit.	Inch lbs. per cu. in.	Work to elastic limit.	Height of drop causing complete failure.	Lbs. per sq. in.	Fiber stress at elastic limit.	Lbs. per sq. in.	Fiber stress at elastic limit.	Maximum crushing strength.	1,000s of lbs. per sq. in.	Lbs. per sq. in.	Modulus of elasticity.	Lbs. per sq. in.		End surface.	Radial surface.	Tangential surface.	Lbs. per sq. in.	Surface of failure radial.	Surface of failure tangential.

III.—ACTUAL VALUE OF EACH PROPERTY FOR EACH "SPECIES-LOCALITY" AS DETERMINED BY TESTS—EXPRESSED IN PERCENTAGE OF EQUATION VALUE—Continued.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30		
CONIFERS—contd.																															
Pine, lodgepole (Granite County, Montana).																															
Green.	41a			105	133	98	94	95	105	90	85	65	100	112	102	101	98	96	140	79	74	85	85	90	85	79	67	68	68		
Air-dry																															
Pine, lodgepole (Jefferson County, Montana).																															
Green.	40a			105	135	105	94	96	112	85	88	86	97	112	96	95	108	103	165	77	74	76	90	90	80	79	66	72	65		
Air-dry																															

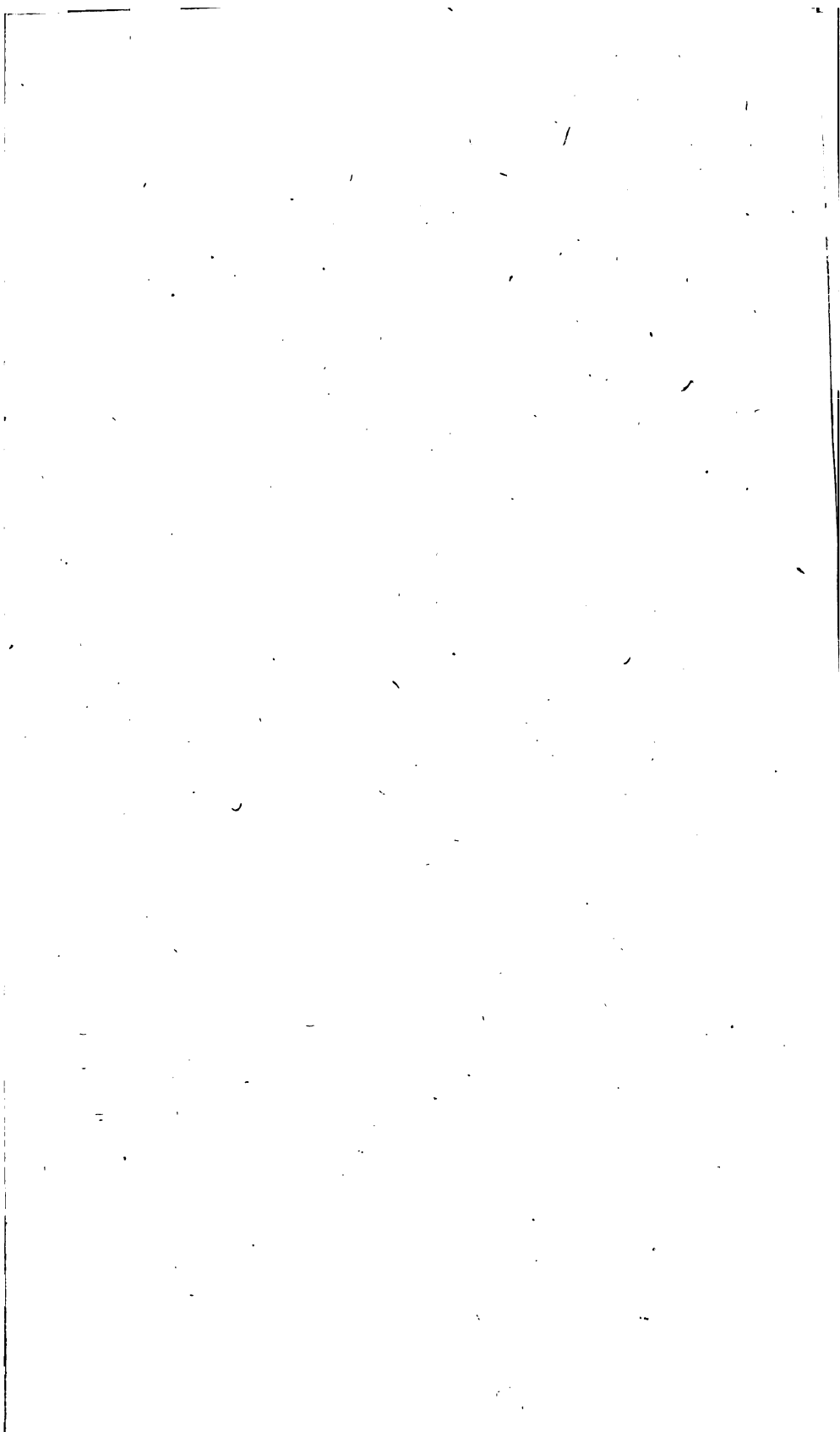
TABLE 1.—Equations and variations—specific gravity, shrinkage, and strength relations based on tests of small clear pieces, green and air-dry—Con.

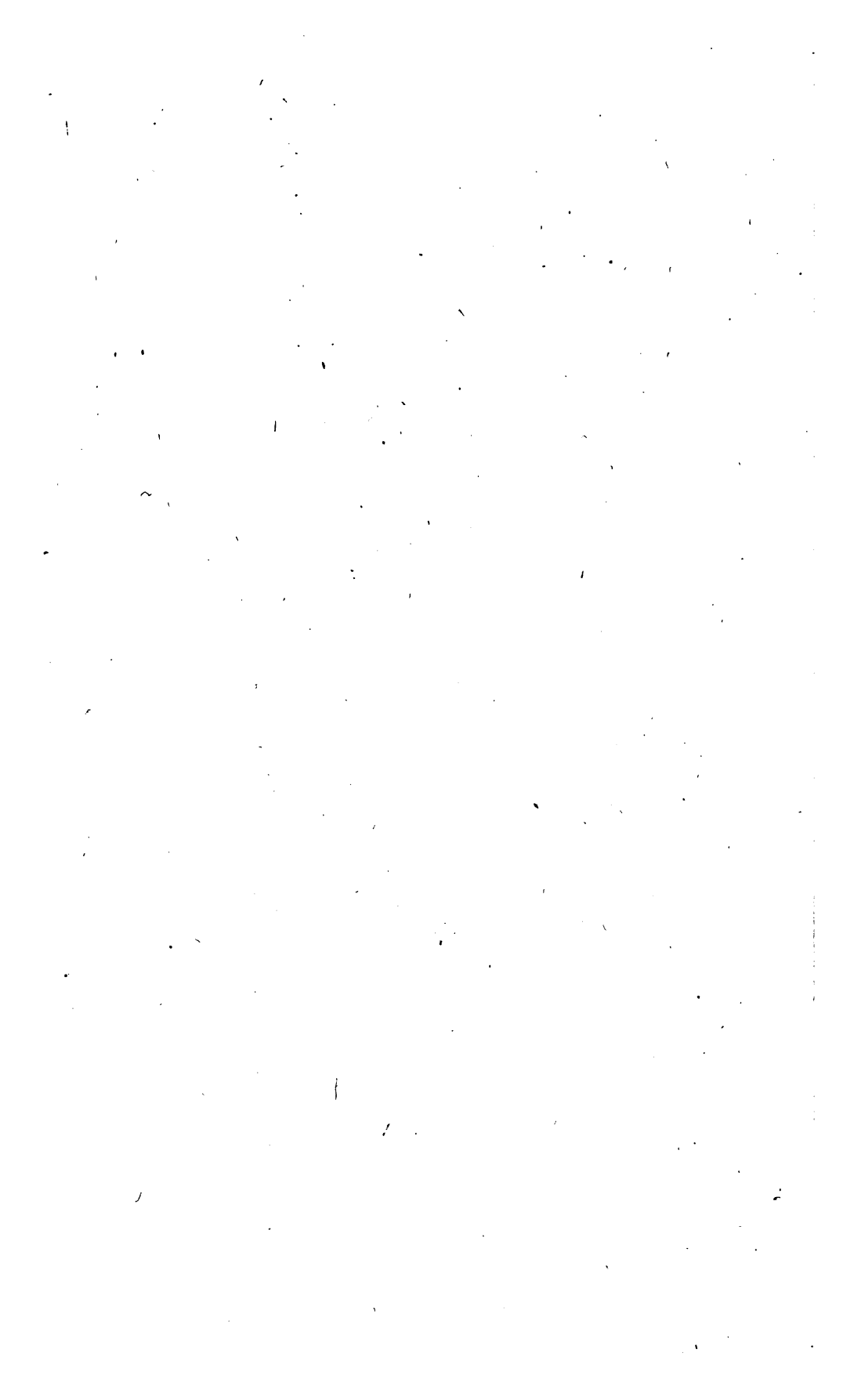
Species and locality.	Reference number.	Specific Gravity, oven-dry, based on volume at time of test.	Per cent.	Moisture content.	Shrinkage from green to oven-dry condition.			Static bending.								Impact bending, 50-pound hammer.						Compression parallel to grain.				Hardness: load required to embed a 0.444-inch ball one-half its diameter.				Shear.		Cleavage.		Tension.		
					In volume.	Radial.	Tangential.	Lbs. per sq. in.	Modulus of rupture.	1,000s of lbs. per sq. in.	Inch lbs. per cu. in.	Work to elastic limit.	Work to maximum load.	Inch lbs. per cu. in.	Total work.	Lbs. per sq. in.	Fiber stress at elastic limit.	Modulus of elasticity.	1,000s of lbs. per sq. in.	Modulus of elasticity.	Work to elastic limit.	Height of drop causing complete failure.	Lbs. per sq. in.	Fiber stress at elastic limit.	Maximum crushing strength.	1,000s of lbs. per sq. in.	Modulus of elasticity.	Compression perpendicular to grain.	Lbs. per sq. in.	End surface.	Radial surface.	Tangential surface.	Lbs. per sq. in.	Surface of failure radial.	Surface of failure tangential.	Lbs. per sq. in.

III.—ACTUAL VALUE OF EACH PROPERTY FOR EACH "SPECIES-LOCALITY" AS DETERMINED BY TESTS—EXPRESSED IN PERCENTAGE OF EQUATION VALUE—Continued.

1.	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	
CONIFERS—contd.																														
Pine, western yellow (Arizona):																														
Green.....	19				91	122	107	90	95	99	86	98	97	94	116	100	103	91	103	90	76	85	88	103	100	112	114	121	114	
Air-dry.....								101	89	135	69	101	84	100	97	72	110	110	92	114	109	112	106	142	128	150	166	142	141	
Pine, western (California):																														
Green.....	37				108	120	114	99	113	95	66	102	100	98	117	105	105	98	118	100	73	79	85	98	93	100	101	83	77	
Air-dry.....								126	106	115	161	141	96	102	109	103	147	113	110	117	81	100	98	100	108	112	112	92	141	
Pine, western (Colorado):																														
Green.....	41				90	102	87	100	104	104	86	73	91	100	90	88	107	97	105	119	71	83	85	92	88	84	74	
Air-dry.....								95	111	99	110	99	110	76	97	73	109	125	110	87	102	92	94	87	98	93	121	103	









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